

Harriott Valentine Engineers Inc.

## STRUCTURAL CALCULATIONS

**Project:**

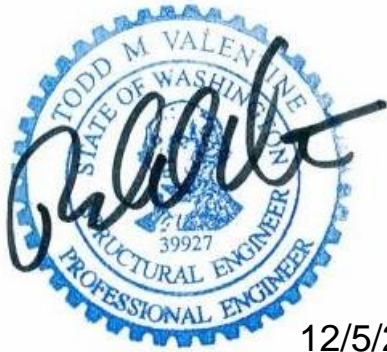
Miles Residence  
8321 SE 83rd St  
Mercer Island, WA 98040

**Architect:**

JML Architects, LLC  
Mercer Island, WA 98040

**Structural Engineer:**

Harriott Valentine Engineers, Inc.  
1932 First Avenue, Suite 720  
Seattle, WA 98101  
tel. 206-624-4760



12/5/24

**SECTION 1: GENERAL**

**CRITERIA**

**Gravity**

roof	dead	asphalt shingles	2.5	live snow	25.0 psf
		1/2" plywood	1.5		
		R30 insulation	1.2		
		(2)2x6 @ 16"oc	3.4		
		5/8" gyp. wallboard	2.8		
		slope factor	2.9		
		miscellaneous	1.7 11%		
			<hr style="width: 100px; margin-left: 0;"/>		
			16.0 psf		
	total	dead + live	41.0 psf		

walls

cement fiber board	4.1
battens 2x2 @ 24"oc	0.3
1/2" plywood	1.5
2x6 @ 16"oc	1.7
R21 insulation	0.8
1/2" gyp. wallboard	2.2 4%
miscellaneous	0.4 psf
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	11.0

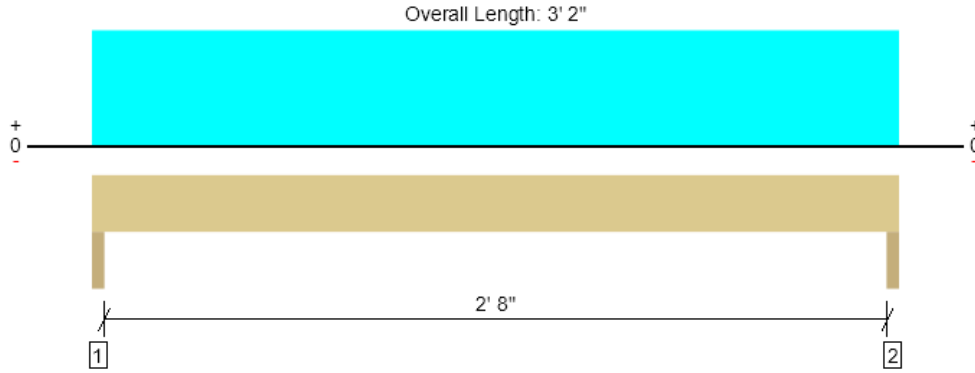
**SECTION 2: FRAMING**

Garage roof			
Member Name	Results (Max UTIL %)	Current Solution	Comments
window header	Passed (7% M)	2 piece(s) 2 x 6 HF No.2	
garage header	Passed (42% M)	1 piece(s) 3 1/2" x 9 1/4" 2.0E Parallam® PSL	
existing ridge	Passed (98% M)	1 piece(s) 4 x 12 DF No.1	
new rafter 1	Passed (54% ΔT)	1 piece(s) 2 x 6 HF No.2 @ 16" OC	
new rafter 2	Passed (91% ΔT)	2 piece(s) 1 3/4" x 5 1/2" 2.0E Microllam® LVL @ 16" OC	
new ridge beam	Passed (87% M)	1 piece(s) 4 x 12 DF No.1	
existing dropped beam	Passed (88% V)	1 piece(s) 4 x 12 DF No.1	

ForteWEB Software Operator	Job Notes
Henry Nuckles Harriott Valentine Engineers (715) 571-0533 HNuckles@harriottvalentine.com	



Garage roof, window header  
**2 piece(s) 2 x 6 HF No.2**



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal (typ.).

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	171 @ 1 1/2"	3645 (3.00")	Passed (5%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	95 @ 8 1/2"	1898	Passed (5%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	115 @ 1' 7"	1602	Passed (7%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.001 @ 1' 7"	0.097	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.003 @ 1' 7"	0.146	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)

Member Length : 3' 2"  
 System : Wall  
 Member Type : Header  
 Building Use : Residential  
 Building Code : IBC 2021  
 Design Methodology : ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Trimmer - HF	3.00"	3.00"	1.50"	122	49	171	None
2 - Trimmer - HF	3.00"	3.00"	1.50"	122	49	171	None

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	3' 2" o/c	
Bottom Edge (Lu)	3' 2" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 3' 2"	N/A	4.2	--	
1 - Uniform (PSF)	0 to 3' 2"	1' 3"	15.0	25.0	Default Load
2 - Uniform (PLF)	0 to 3' 2"	N/A	54.0	-	

**Weyerhaeuser Notes**

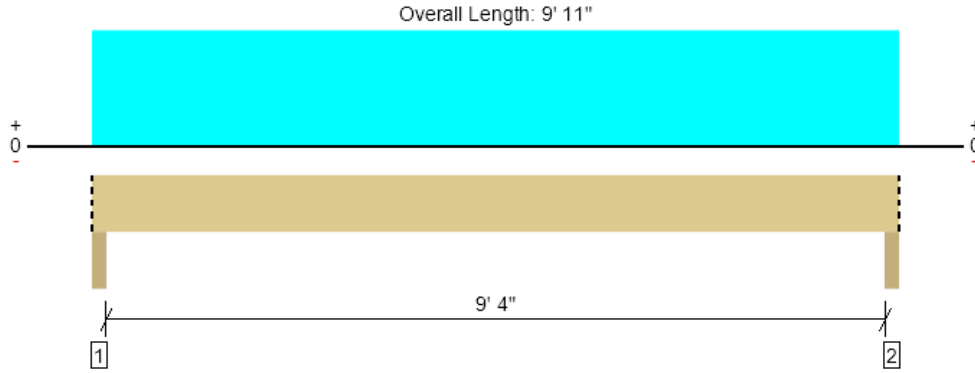
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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
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Garage roof, garage header  
**1 piece(s) 3 1/2" x 9 1/4" 2.0E Parallam® PSL**



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal (typ.).

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	2613 @ 2"	7656 (3.50")	Passed (34%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	2053 @ 1' 3/4"	7198	Passed (29%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	6049 @ 4' 11 1/2"	14278	Passed (42%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.146 @ 4' 11 1/2"	0.479	Passed (L/788)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.238 @ 4' 11 1/2"	0.639	Passed (L/483)	--	1.0 D + 1.0 S (All Spans)

Member Length : 9' 11"  
 System : Roof  
 Member Type : Drop Beam  
 Building Use : Residential  
 Building Code : IBC 2021  
 Design Methodology : ASD  
 Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Column - HF	3.50"	3.50"	1.50"	1011	1602	2613	Blocking
2 - Column - HF	3.50"	3.50"	1.50"	1011	1602	2613	Blocking

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	9' 11" o/c	
Bottom Edge (Lu)	9' 11" o/c	

- Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 9' 11"	N/A	10.1	--	
1 - Uniform (PSF)	0 to 9' 11" (Front)	12' 11 1/16"	15.0	25.0	Default Load

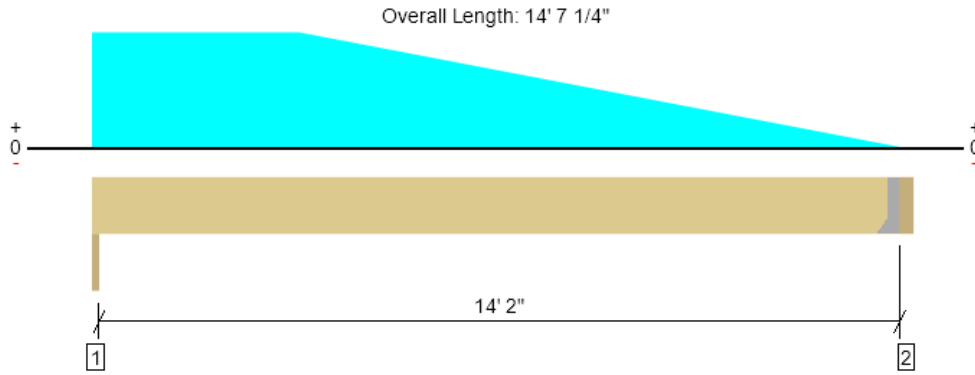
- Side loads are assumed to not induce cross-grain tension.

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Garage roof, existing ridge  
**1 piece(s) 4 x 12 DF No.1**



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal (typ.).

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	2562 @ 1/4"	3828 (1.75")	Passed (67%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	2092 @ 1' 1"	5434	Passed (39%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	7594 @ 6' 2 1/8"	7783	Passed (98%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.227 @ 6' 11"	0.715	Passed (L/754)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.386 @ 6' 11 1/8"	0.953	Passed (L/444)	--	1.0 D + 1.0 S (All Spans)

Member Length : 14' 3 3/4"  
 System : Roof  
 Member Type : Drop Beam  
 Building Use : Residential  
 Building Code : IBC 2021  
 Design Methodology : ASD  
 Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Column - HF	1.75"	1.75"	1.50"	1043	1519	2562	None
2 - Hanger on 11 1/4" HF beam	3.50"	Hanger <sup>1</sup>	1.50"	601	828	1430	See note <sup>1</sup>

- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- <sup>1</sup> See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	9' 5" o/c	
Bottom Edge (Lu)	14' 4" o/c	

- Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie							
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories	
2 - Face Mount Hanger	LUS410	2.00"	N/A	8-10d	6-10d		

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 14' 3 3/4"	N/A	10.0	--	
1 - Uniform (PSF)	0 to 3' 9" (Front)	10' 4"	16.0	25.0	Default Load
2 - Tapered (PSF)	3' 9" to 14' 5" (Front)	10' 4" to 0	16.0	25.0	

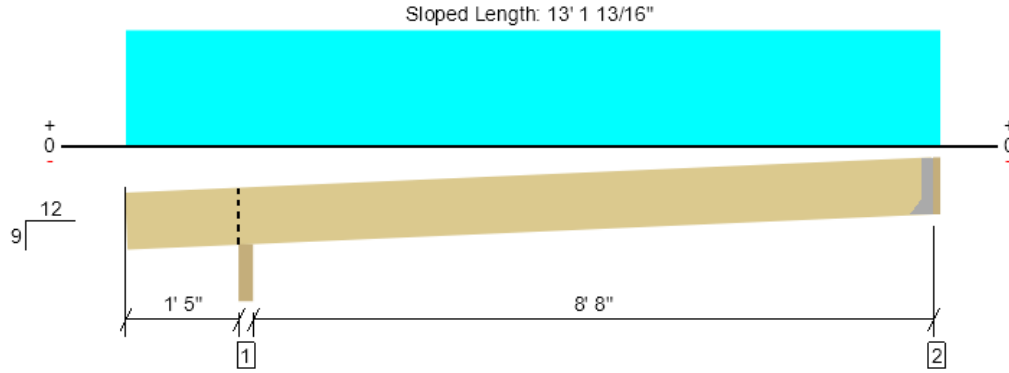
- Side loads are assumed to not induce cross-grain tension.

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ForteWEB Software Operator	Job Notes
Henry Nuckles Harriott Valentine Engineers (715) 571-0533 HNuckles@harriottvalentine.com	



Garage roof, new rafter 1  
**1 piece(s) 2 x 6 HF No.2 @ 16" OC**



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal (typ.).

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	230 @ 10' 4 1/2"	911 (1.50")	Passed (25%)	--	1.0 D + 1.0 S (Alt Spans)
Shear (lbs)	215 @ 2' 7/8"	949	Passed (23%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	496 @ 6' 3/4"	921	Passed (54%)	1.15	1.0 D + 1.0 S (Alt Spans)
Live Load Defl. (in)	0.252 @ 5' 11 7/8"	0.551	Passed (L/525)	--	1.0 D + 1.0 S (Alt Spans)
Total Load Defl. (in)	0.397 @ 6'	0.734	Passed (L/333)	--	1.0 D + 1.0 S (Alt Spans)

Member Length : 13' 3 3/4"  
 System : Roof  
 Member Type : Joist  
 Building Use : Residential  
 Building Code : IBC 2021  
 Design Methodology : ASD  
 Member Pitch : 9/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Overhang deflection criteria: LL (2L/240) and TL (2L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A 15% increase in the moment capacity has been added to account for repetitive member usage.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Beveled Plate - SPF	3.50"	3.50"	1.50"	122	204	326	Blocking
2 - Hanger on 5 1/2" HF beam	1.75"	Hanger <sup>1</sup>	1.50"	88	149	237	See note <sup>1</sup>

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- <sup>1</sup> See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	12' 7" o/c	
Bottom Edge (Lu)	13' o/c	

- Maximum allowable bracing intervals based on applied load.
- Dimensions for lateral bracing intervals are measured along the length of the member for sloped conditions.

**Connector: Simpson Strong-Tie**

Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories
2 - Face Mount Hanger	LRU26Z	1.94"	N/A	4-10dx1.5	5-10d	

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Load	Location (Side)	Spacing	Dead (0.90)	Snow (1.15)	Comments
1 - Uniform (PSF)	0 to 10' 6 1/4"	16"	12.0	25.0	Default Load

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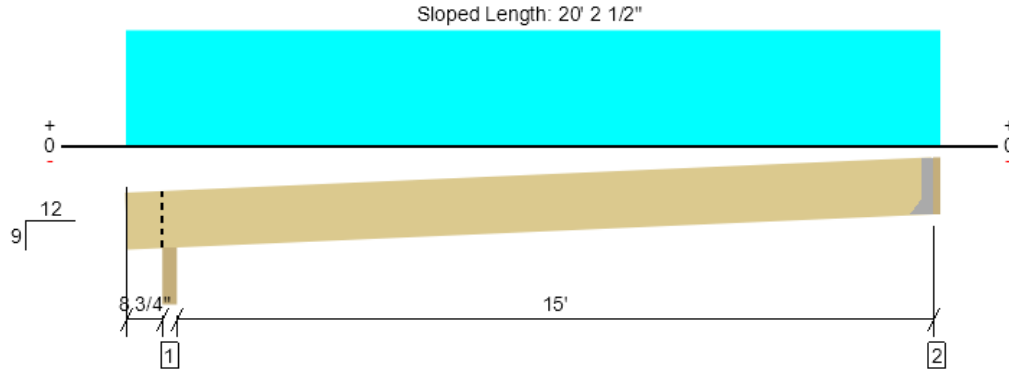
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Garage roof, new rafter 2

**2 piece(s) 1 3/4" x 5 1/2" 2.0E Microllam® LVL @ 16" OC**



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal (typ.).

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	453 @ 16' 1/4"	3938 (1.50")	Passed (12%)	--	1.0 D + 1.0 S (Alt Spans)
Shear (lbs)	431 @ 15' 7 7/8"	4206	Passed (10%)	1.15	1.0 D + 1.0 S (Alt Spans)
Moment (Ft-lbs)	1712 @ 8' 5 5/8"	5084	Passed (34%)	1.15	1.0 D + 1.0 S (Alt Spans)
Live Load Defl. (in)	0.639 @ 8' 5 7/16"	0.947	Passed (L/356)	--	1.0 D + 1.0 S (Alt Spans)
Total Load Defl. (in)	1.147 @ 8' 5 7/16"	1.262	Passed (L/198)	--	1.0 D + 1.0 S (Alt Spans)

Member Length : 20' 4 7/16"  
 System : Roof  
 Member Type : Joist  
 Building Use : Residential  
 Building Code : IBC 2021  
 Design Methodology : ASD  
 Member Pitch : 9/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Overhang deflection criteria: LL (2L/240) and TL (2L/180).
- Upward deflection on left cantilever exceeds overhang deflection criteria.
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A 4% increase in the moment capacity has been added to account for repetitive member usage.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Beveled Plate - SPF	3.50"	3.50"	1.50"	226	282	508	Blocking
2 - Hanger on 5 1/2" HF beam	1.75"	Hanger <sup>1</sup>	1.50"	204	257	461	See note <sup>1</sup>

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- <sup>1</sup> See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	20' o/c	
Bottom Edge (Lu)	20' o/c	

- Maximum allowable bracing intervals based on applied load.
- Dimensions for lateral bracing intervals are measured along the length of the member for sloped conditions.

**Connector: Simpson Strong-Tie**

Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories
2 - Face Mount Hanger	U46X SLD36	2.00"	N/A	8-10dx1.5	4-10d	

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Load	Location (Side)	Spacing	Dead (0.90)	Snow (1.15)	Comments
1 - Uniform (PSF)	0 to 16' 2"	16"	16.0	25.0	Default Load

**Weyerhaeuser Notes**

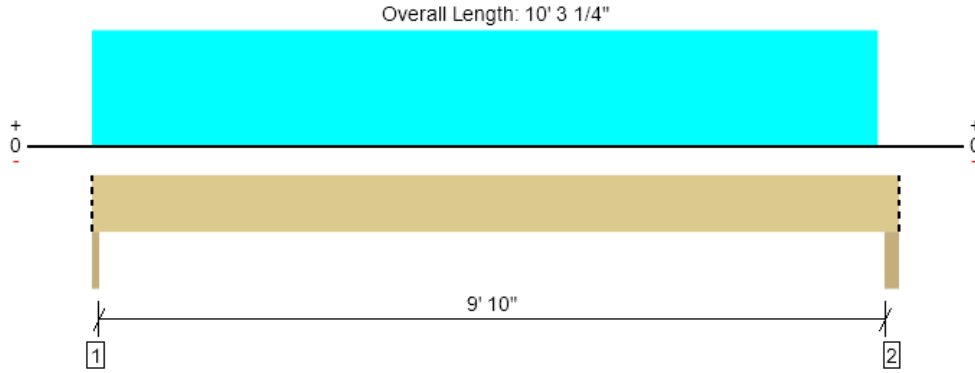
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Garage roof, new ridge beam  
**1 piece(s) 4 x 12 DF No.1**



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal (typ.).

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	2700 @ 1/4"	3828 (1.75")	Passed (71%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	2123 @ 9' 1/2"	5434	Passed (39%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	6779 @ 5' 3/4"	7783	Passed (87%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.100 @ 5' 3/4"	0.504	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.176 @ 5' 3/4"	0.672	Passed (L/689)	--	1.0 D + 1.0 S (All Spans)

Member Length : 10' 3 1/4"  
 System : Roof  
 Member Type : Drop Beam  
 Building Use : Residential  
 Building Code : IBC 2021  
 Design Methodology : ASD  
 Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Column - HF	1.75"	1.75"	1.50"	1159	1541	2700	Blocking
2 - Column - HF	3.50"	3.50"	1.50"	1133	1504	2637	Blocking

• Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	10' 3" o/c	
Bottom Edge (Lu)	10' 3" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 10' 3 1/4"	N/A	10.0	--	
1 - Uniform (PLF)	0 to 10' (Front)	N/A	66.0	111.8	Linked from: new rafter 1, Support 2
2 - Uniform (PLF)	0 to 10' (Back)	N/A	153.0	192.8	Linked from: new rafter 2, Support 2

• Side loads are assumed to not induce cross-grain tension.

**Weyerhaeuser Notes**

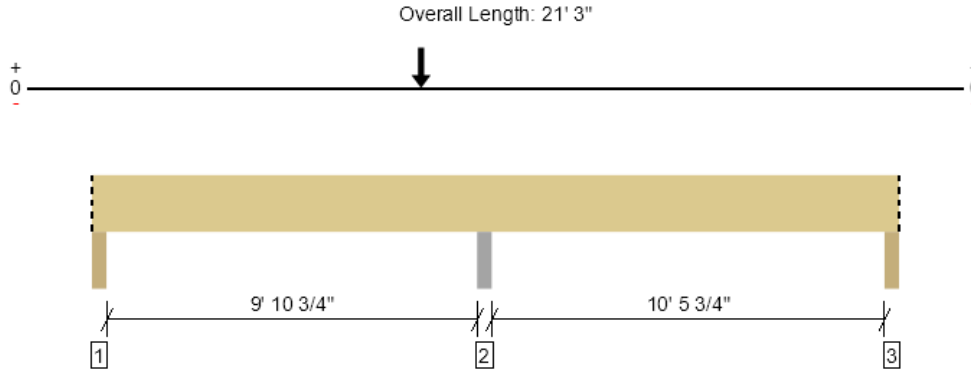
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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
Henry Nuckles Harriott Valentine Engineers (715) 571-0533 HNNuckles@harriottvalentine.com	



Garage roof, existing dropped beam  
**1 piece(s) 4 x 12 DF No.1**



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal (typ.).

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	5156 @ 10' 4"	7656 (3.50")	Passed (67%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	4775 @ 9' 3"	5434	Passed (88%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	4553 @ 8' 8"	7783	Passed (59%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.049 @ 5' 10 1/4"	0.508	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.085 @ 5' 9 15/16"	0.678	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)

Member Length : 21' 3"  
 System : Roof  
 Member Type : Drop Beam  
 Building Use : Residential  
 Building Code : IBC 2021  
 Design Methodology : ASD  
 Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- -262 lbs uplift at support located at 21' 1". Strapping or other restraint may be required.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Column - HF	3.50"	3.50"	1.50"	265	314	580	Blocking
2 - Column - steel	3.50"	3.50"	2.36"	2234	2922	5156	None
3 - Column - HF	3.50"	3.50"	1.50"	-85	-177	-262	Blocking

• Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	21' 3" o/c	
Bottom Edge (Lu)	21' 3" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 21' 3"	N/A	10.0	--	
1 - Point (lb)	8' 8" (Top)	N/A	1043	1519	Linked from: existing ridge, Support 1
2 - Point (lb)	8' 8" (Top)	N/A	1159	1541	Linked from: new ridge beam, Support 1

• Side loads are assumed to not induce cross-grain tension.

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
Henry Nuckles Harriott Valentine Engineers (715) 571-0533 HNuckles@harriottvalentine.com	



**SECTION 3: LATERAL**

⚠ This is a beta release of the new ATC Hazards by Location website. Please [contact us](#) with feedback.

ℹ The ATC Hazards by Location website will not be updated to support ASCE 7-22. [Find out why.](#)

# ATC Hazards by Location

## Search Information

**Address:** 8321 SE 83rd St, Mercer Island, WA 98040, USA  
**Coordinates:** 47.5289906, -122.228952  
**Elevation:** 257 ft  
**Timestamp:** 2024-11-20T20:31:56.968Z  
**Hazard Type:** Seismic  
**Reference Document:** ASCE7-16  
**Risk Category:** II  
**Site Class:** D-default



## Basic Parameters

Name	Value	Description
$S_S$	1.468	$MCE_R$ ground motion (period=0.2s)
$S_1$	0.506	$MCE_R$ ground motion (period=1.0s)
$S_{MS}$	1.761	Site-modified spectral acceleration value
$S_{M1}$	* null	Site-modified spectral acceleration value
$S_{DS}$	1.174	Numeric seismic design value at 0.2s SA
$S_{D1}$	* null	Numeric seismic design value at 1.0s SA

\* See Section 11.4.8

## Additional Information

Name	Value	Description
SDC	* null	Seismic design category
$F_a$	1.2	Site amplification factor at 0.2s
$F_v$	* null	Site amplification factor at 1.0s
$CR_S$	0.902	Coefficient of risk (0.2s)
$CR_1$	0.898	Coefficient of risk (1.0s)
PGA	0.628	$MCE_G$ peak ground acceleration
$F_{PGA}$	1.2	Site amplification factor at PGA
$PGA_M$	0.753	Site modified peak ground acceleration
$T_L$	6	Long-period transition period (s)
$SsRT$	1.468	Probabilistic risk-targeted ground motion (0.2s)
$SsUH$	1.627	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
$SsD$	4.32	Factored deterministic acceleration value (0.2s)
$S1RT$	0.506	Probabilistic risk-targeted ground motion (1.0s)
$S1UH$	0.563	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
$S1D$	1.634	Factored deterministic acceleration value (1.0s)
$PGAd$	1.422	Factored deterministic acceleration value (PGA)

\* See Section 11.4.8

The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

Please note that the ATC Hazards by Location website will not be updated to support ASCE 7-22. [Find out why.](#)

## Disclaimer

Hazard loads are provided by the U.S. Geological Survey [Seismic Design Web Services](#).

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## SEISMIC DESIGN

ASCE 7-16  
Equivalent Lateral Force Procedure

RISK Category	II	Table 1.5-1
Seismic Design Category	D	Table 11.6-1
Importance Factor	1.00	Table 1.5-2
Site Class	D	Table 20.3-1 <b>per Geotech or DEFAULT</b>
S <sub>s</sub>	146.80 %g	(from SEAOC/OSHPD website tool)
S <sub>1</sub>	50.60 %g	(from SEAOC/OSHPD website tool)
F <sub>a</sub>	1.20	Table 11.4-1 <b>USE Fa=1.2 for DEFAULT Site Class D</b>
F <sub>v</sub>	1.80	Table 11.4-2
C <sub>t</sub>	0.02	Table 12.8-2
x	0.75	Table 12.8-2
h <sub>n</sub>	30.00 feet	(height to highest level)
S <sub>MS</sub> = F <sub>a</sub> *S <sub>s</sub>	1.7616	Eq. 11.4-1
S <sub>M1</sub> = F <sub>v</sub> *S <sub>1</sub>	0.9108	Eq. 11.4-2
S <sub>DS</sub> = (2/3)*S <sub>MS</sub>	1.1744 g	Eq. 11.4-3
S <sub>D1</sub> = (2/3)*S <sub>M1</sub>	0.6072 g	Eq. 11.4-4
Period T <sub>a</sub> = C <sub>t</sub> *h <sub>n</sub> <sup>x</sup>	0.2564 s	Eq. 12.8-7
T <sub>o</sub>	0.1034 s	per section 11.4.6
T <sub>s</sub>	0.5170 s	per section 11.4.6
S <sub>a</sub>	1.1744 g	per section 11.4.6
R	6.5	Table 12.2-1
Ω <sub>o</sub>	2.5	Table 12.2-1
C <sub>d</sub>	4	Table 12.2-1
Section 12.8 (ELF) ok?	Yes	Table 12.6-1

Equivalent Lateral Force Procedure (section 12.8)

C <sub>s</sub>	0.1807	Eq. 12.8-2
W, weight	8,125 lb	per table below
Q <sub>E</sub>	1,468 lb	Eq. 12.8-1

Vertical Force Distribution (section 12.8.3)

k = 1.00

Level	Hx (ft)	Floor Area (ft <sup>2</sup> )	Seismic Dead Ld (psf)	Floor Wt. (k)	Wall Length (ft)	Wall Wt. (k)	Total Wt. (k)	WxHx (k-ft)	Cvx (%)	(LRFD) Q <sub>E</sub> (k)	(ASD) 0.7Q <sub>E</sub> (k)
Garage Roof	15.88	330	15	5.0	50	3.2	8.1	129.0	100.0	1.47	1.03
							8.13	128.98	100.00	1.47	<b>1.03</b>

## WIND DESIGN

ASCE 7-10

Simplified Envelope Method (Chapter 28)

$$p_s = \lambda K_{zt} I p_{s30}$$

$$\lambda = \text{adjustment factor} = 1.49$$

$$I = \text{importance factor} = 1.00$$

$$K_{zt} = \text{topographic factor} = 1.90$$

Part of Figure 28.6-1 - Adjustment Factor for Building Height and Exposure,  $\lambda$

Mean Roof Height (ft)	Exposure		
	B	C	D
15	1.00	1.21	<b>1.47</b>
16	1.00	1.23	<b>1.49</b>
17	1.00	1.24	<b>1.50</b>
18	1.00	1.26	<b>1.52</b>
19	1.00	1.27	<b>1.53</b>
20	1.00	1.29	<b>1.55</b>
21	1.00	1.30	<b>1.56</b>
22	1.00	1.31	<b>1.57</b>
23	1.00	1.33	<b>1.59</b>
24	1.00	1.34	<b>1.60</b>
25	1.00	1.35	<b>1.61</b>
26	1.00	1.36	<b>1.62</b>
27	1.00	1.37	<b>1.63</b>
28	1.00	1.38	<b>1.64</b>
29	1.00	1.39	<b>1.65</b>
30	1.00	1.40	<b>1.66</b>

Zone  
Computation

a = 10% of least horizontal dimension or 0.4 x h, whichever is smaller, but not less than either 4% of least horizontal dimension or 3 feet.

$$w = 24.50 \text{ ft} \times 0.1 = 2.45 \text{ ft}$$

$$h = 16.00 \text{ ft} \times 0.4 = 6.40 \text{ ft}$$

$$w = 24.50 \text{ ft} \times 0.04 = 0.98 \text{ ft}$$

$$a = 3.00 \text{ ft}$$

$$2a = 6.00 \text{ ft}$$

Zone B - end zone of roof

Zone A - end zone of wall

Zone D - interior zone of roof

Zone C - interior zone of wall

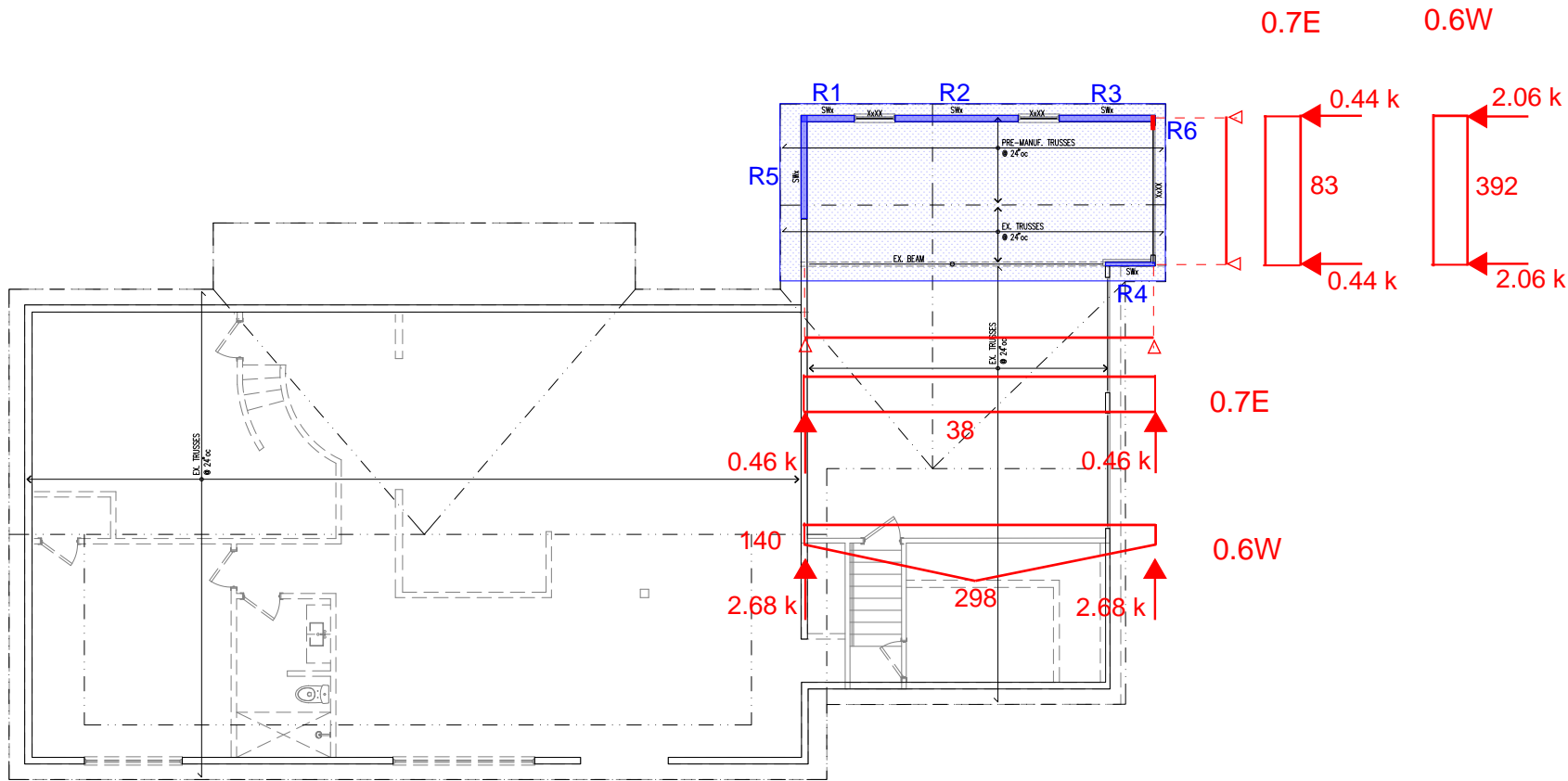
Part of Figure 28.6-1 - Method 2  
Design Wind Pressure,  $p_{s30}$

Basic Speed	Roof Angle	Roof Pitch	Horizontal Pressures (psf)			
			A	B	C	D
100	0 to 5	flat	15.9	-8.2	10.5	-4.9
	10	2	17.9	-7.4	11.9	-4.3
	15	3	19.9	-6.6	13.3	-3.8
	20	4	22.0	-5.8	14.6	-3.2
	25	6	19.9	3.2	14.4	3.3
	30 to 45	7 to 12	17.8	12.2	14.2	9.8

Design Wind Pressure, ps

Basic Speed	Roof Angle	Roof Pitch	Horizontal Pressures (psf)			
			A	B	C	D
100	0 to 5	flat	45.0	-23.2	29.7	-13.9
	10	2	50.7	-20.9	33.7	-12.2
	15	3	56.3	-18.7	37.7	-10.8
	20	4	62.3	-16.4	41.3	-9.1
	25	6	56.3	9.1	40.8	9.3
	30 to 45	7 to 12	50.4	34.5	40.2	27.7

<<<



# Garage Roof Lateral Load Distribution

**LATERAL FORCE DISTRIBUTION**

**East-West**

Walls Below Roof

va' = allowable shear values multiplied by (1.25-0.125 \* h/l)  
for wall aspect ratios greater than 2:1, and only for seismic

  = Simpson Strongwall - not designed here

WALL	WIND				SEISMIC							SW	SW	M <sub>ot</sub> (lbft)	M <sub>ot</sub> (abv)	M <sub>ot</sub> (total)	OT (lb)	DL max		I	HD	TL (lb)	C (lb)	POST	
	L (ft)	h (ft)	h/l	F (lb)	V (abv)	V (total)	v (plf)	F (lb)	V (abv)	V (total)	v (plf)							va'	DL max (lb)						DL max (lb)
R1	3.67	9.25	2.52	409	0	409	111	SW1	87	0	87	31	33	SW1	SW1	3780	0	3780	1030	112	918	HDU2	0	1030	(2)2x4
																3780	0	3780	1030	112	918	HDU2	0	1030	(2)2x4
R2	8.50	13.50	1.59	946	0	946	111	SW1	202	0	202	31	N/A	SW1	SW1	12778	0	12778	1503	358	1146	HDU2	0	1503	(2)2x4
																12778	0	12778	1503	358	1146	HDU2	0	1503	(2)2x4
R3	6.33	8.50	1.34	705	0	705	111	SW1	151	0	151	31	N/A	SW1	SW1	5991	0	5991	946	181	766	HDU2	0	946	(2)2x4
																5991	0	5991	946	181	766	HDU2	0	946	(2)2x4
R4	3.50	8.50	2.43	1	0	1	0	SW1	1	0	1	0	0	SW1	SW1	9	0	9	2	100	-98	--	0	2	(2)2x4
																9	0	9	2	100	-98	--	0	2	(2)2x4

**North-South**

Walls Below Roof

WALL	WIND				SEISMIC							SW	SW	M <sub>ot</sub> (lbft)	M <sub>ot</sub> (abv)	M <sub>ot</sub> (total)	OT (lb)	DL max		I	HD	TL (lb)	C (lb)	POST	
	L (ft)	h (ft)	h/l	F (lb)	V (abv)	V (total)	v (plf)	F (lb)	V (abv)	V (total)	v (plf)							va'	DL max (lb)						DL max (lb)
R5	7.25	9.25	1.28	2680	0	2680	370	SW2	460	0	460	82	N/A	SW1	SW2	24790	0	24790	3419	630	2790	HDU4	0	3419	(2)2x4
																24790	0	24790	3419	630	2790	HDU4	0	3419	(2)2x4
<span style="background-color: yellow;">R6</span>	1.50	6.50	4.33	2680	0	2680	1787	--	1	0	1	1	1	--	--	17420	0	17420	11613	57	11556	--	0	11613	--
																17420	0	17420	11613	57	11556	--	0	11613	--

rho = 1.30 per ASCE 7-10 12.3.4.2

**SECTION 4: FOUNDATION**



# HDU2 (Cast in)

## 1. Project information

Customer company:  
Customer contact name:  
Customer e-mail:  
Comment:

Project description: HDU2 Cast In

LRFD Loads

1.0W = 1146 lb

Location:

Fastening description:

## 2. Input Data & Anchor Parameters

### General

Design method: ACI 318-14  
Units: Imperial units

### Anchor Information:

Anchor type: Cast-in-place  
Material: AB  
Diameter (inch): 0.625  
Effective Embedment depth,  $h_{ef}$  (inch): 6.000  
Anchor category: -  
Anchor ductility: Yes  
 $h_{min}$  (inch): 8.13  
 $C_{min}$  (inch): 1.38  
 $S_{min}$  (inch): 2.50

### Base Material

Concrete: Normal-weight  
Concrete thickness,  $h$  (inch): 24.00  
State: Cracked  
Compressive strength,  $f'_c$  (psi): 2500  
 $\Psi_{c,v}$ : 1.0  
Reinforcement condition: B tension, B shear  
Supplemental reinforcement: Not applicable  
Reinforcement provided at corners: Yes  
Ignore concrete breakout in tension: No  
Ignore concrete breakout in shear: No  
Ignore 6do requirement: Yes  
Build-up grout pad: No

### Recommended Anchor

Anchor Name: PAB Pre-Assembled Anchor Bolt - PAB5 (5/8"Ø)



**Load and Geometry**

Load factor source: ACI 318 Section 5.3

Load combination: not set

Seismic design: No

Anchors subjected to sustained tension: Not applicable

Apply entire shear load at front row: No

Anchors only resisting wind and/or seismic loads: Yes

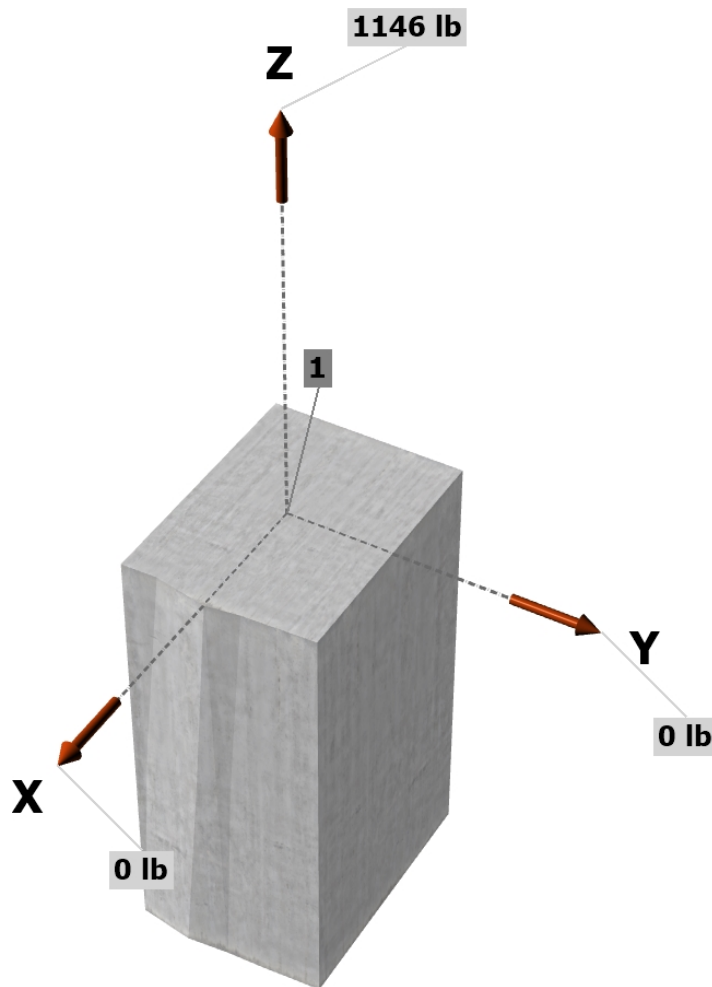
Strength level loads:

$N_{ua}$  [lb]: 1146

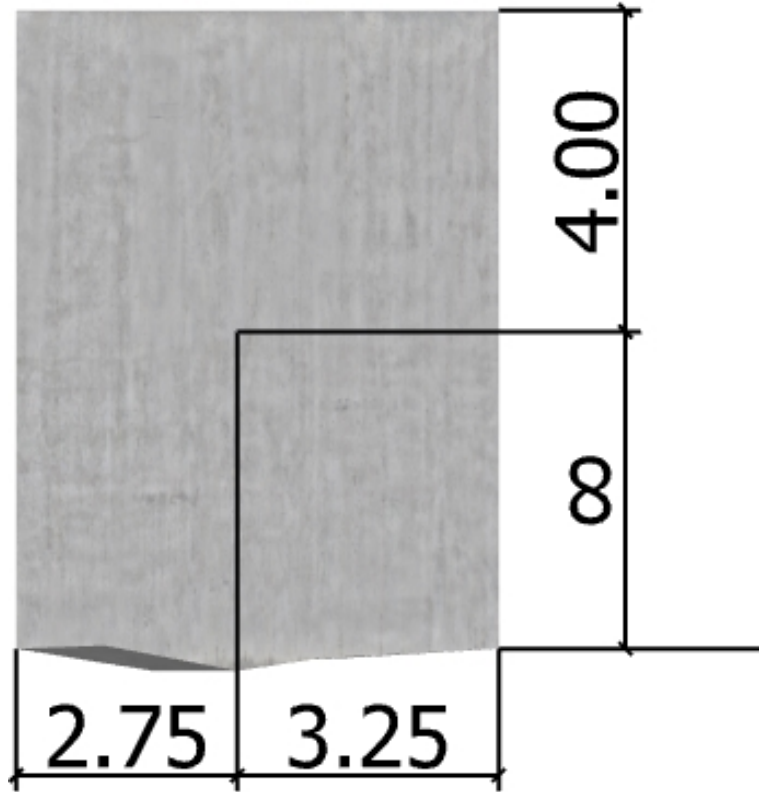
$V_{uax}$  [lb]: 0

$V_{uay}$  [lb]: 0

<Figure 1>



<Figure 2>





### 3. Resulting Anchor Forces

Anchor	Tension load, N <sub>ua</sub> (lb)	Shear load x, V <sub>uax</sub> (lb)	Shear load y, V <sub>uay</sub> (lb)	Shear load combined, $\sqrt{(V_{uax})^2 + (V_{uay})^2}$ (lb)
1	1146.0	0.0	0.0	0.0
Sum	1146.0	0.0	0.0	0.0

Maximum concrete compression strain (%): 0.00  
 Maximum concrete compression stress (psi): 0  
 Resultant tension force (lb): 1146  
 Resultant compression force (lb): 0  
 Eccentricity of resultant tension forces in x-axis, e'<sub>Nx</sub> (inch): 0.00  
 Eccentricity of resultant tension forces in y-axis, e'<sub>Ny</sub> (inch): 0.00

### 4. Steel Strength of Anchor in Tension (Sec. 17.4.1)

N <sub>sa</sub> (lb)	φ	φN <sub>sa</sub> (lb)
13100	0.75	9825

### 5. Concrete Breakout Strength of Anchor in Tension (Sec. 17.4.2)

$$N_b = k_c \lambda_a \sqrt{f_c} h_{ef}^{1.5} \text{ (Eq. 17.4.2.2a)}$$

k <sub>c</sub>	λ <sub>a</sub>	f <sub>c</sub> (psi)	h <sub>ef</sub> (in)	N <sub>b</sub> (lb)
24.0	1.00	2500	2.667	5226

$$\phi N_{cb} = \phi (A_{Nc} / A_{Nco}) \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b \text{ (Sec. 17.3.1 \& Eq. 17.4.2.1a)}$$

A <sub>Nc</sub> (in <sup>2</sup> )	A <sub>Nco</sub> (in <sup>2</sup> )	c <sub>a,min</sub> (in)	Ψ <sub>ed,N</sub>	Ψ <sub>c,N</sub>	Ψ <sub>cp,N</sub>	N <sub>b</sub> (lb)	φ	φN <sub>cb</sub> (lb)
53.25	64.00	2.75	0.906	1.00	1.000	5226	0.70	2758

### 6. Pullout Strength of Anchor in Tension (Sec. 17.4.3)

$$\phi N_{pn} = \phi \Psi_{c,P} N_p = \phi \Psi_{c,P} 8 A_{brg} f_c \text{ (Sec. 17.3.1, Eq. 17.4.3.1 \& 17.4.3.4)}$$

Ψ <sub>c,P</sub>	A <sub>brg</sub> (in <sup>2</sup> )	f <sub>c</sub> (psi)	φ	φN <sub>pn</sub> (lb)
1.0	2.10	2500	0.70	29372



**11. Results**

**11. Interaction of Tensile and Shear Forces (Sec. D.7)?**

Tension	Factored Load, $N_{ua}$ (lb)	Design Strength, $\phi N_n$ (lb)	Ratio	Status
Steel	1146	9825	0.12	Pass
<b>Concrete breakout</b>	<b>1146</b>	<b>2758</b>	<b>0.42</b>	<b>Pass (Governs)</b>
Pullout	1146	29372	0.04	Pass

**PAB5 (5/8"Ø) with hef = 6.000 inch meets the selected design criteria.**

**12. Warnings**

- Minimum spacing and edge distance requirement of  $6d_a$  per ACI 318 Sections 17.7.1 and 17.7.2 for torqued cast-in-place anchor is waived per designer option.
- Designer must exercise own judgement to determine if this design is suitable.



# HDU2 (Epoxy)

## 1. Project information

Customer company:  
Customer contact name:  
Customer e-mail:  
Comment:

Project description: HDU2 Epoxy

LRFD Loads

1.0W = 1146 lb

Location:

Fastening description:

## 2. Input Data & Anchor Parameters

### General

Design method: ACI 318-14  
Units: Imperial units

### Anchor Information:

Anchor type: Bonded anchor  
Material: F1554 Grade 36  
Diameter (inch): 0.625  
Effective Embedment depth,  $h_{ef}$  (inch): 6.000  
Code report: ICC-ES ESR-4057  
Anchor category: -  
Anchor ductility: Yes  
 $h_{min}$  (inch): 7.38  
 $c_{ac}$  (inch): 9.44  
 $c_{min}$  (inch): 1.75  
 $s_{min}$  (inch): 3.00

### Base Material

Concrete: Normal-weight  
Concrete thickness,  $h$  (inch): 24.00  
State: Cracked  
Compressive strength,  $f'_c$  (psi): 2500  
 $\Psi_{c,v}$ : 1.0  
Reinforcement condition: B tension, B shear  
Supplemental reinforcement: Not applicable  
Reinforcement provided at corners: Yes  
Ignore concrete breakout in tension: No  
Ignore concrete breakout in shear: No  
Hole condition: Dry concrete  
Inspection: Continuous  
Temperature range, Short/Long: 150/110°F  
Ignore 6do requirement: Not applicable  
Build-up grout pad: No

### Recommended Anchor

Anchor Name: SET-3G - SET-3G w/ 5/8"Ø F1554 Gr. 36  
Code Report: ICC-ES ESR-4057



**Load and Geometry**

Load factor source: ACI 318 Section 5.3

Load combination: not set

Seismic design: No

Anchors subjected to sustained tension: No

Apply entire shear load at front row: No

Anchors only resisting wind and/or seismic loads: Yes

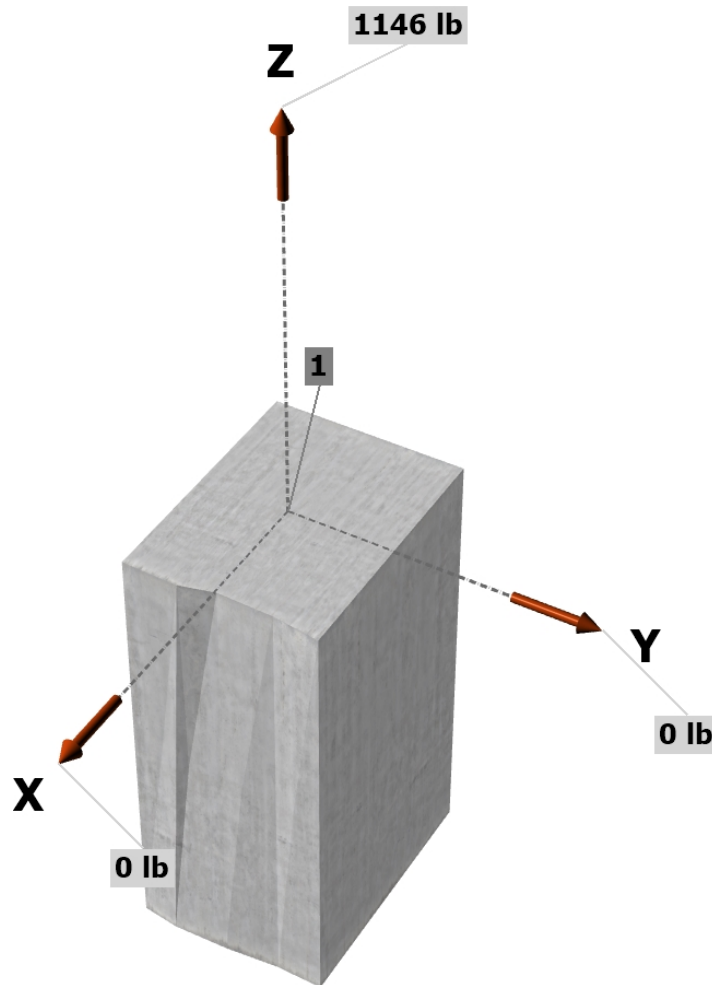
Strength level loads:

$N_{ua}$  [lb]: 1146

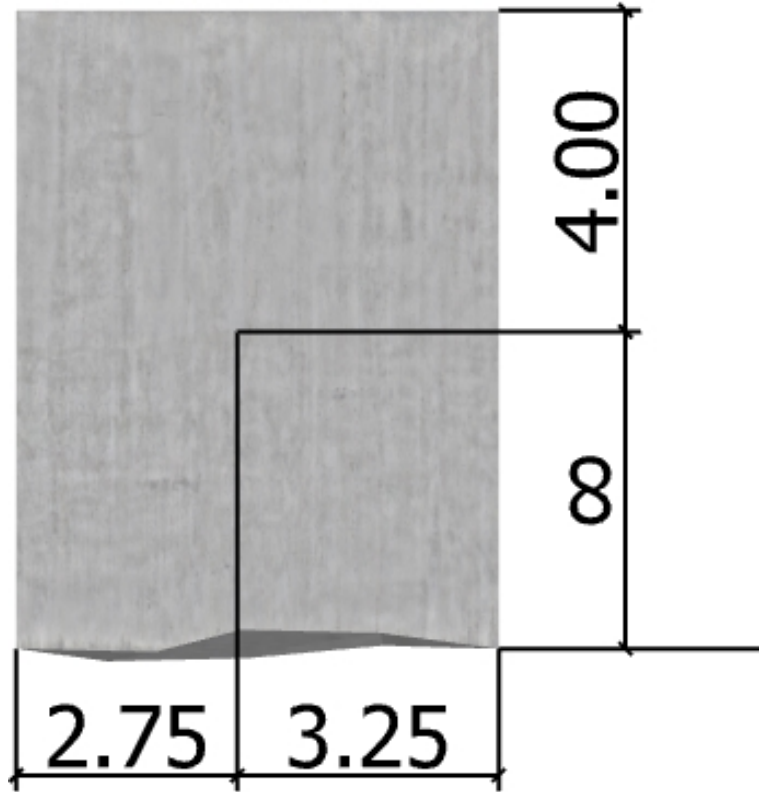
$V_{uax}$  [lb]: 0

$V_{uay}$  [lb]: 0

<Figure 1>



<Figure 2>





### 3. Resulting Anchor Forces

Anchor	Tension load, $N_{ua}$ (lb)	Shear load x, $V_{uax}$ (lb)	Shear load y, $V_{uay}$ (lb)	Shear load combined, $\sqrt{(V_{uax})^2 + (V_{uay})^2}$ (lb)
1	1146.0	0.0	0.0	0.0
Sum	1146.0	0.0	0.0	0.0

Maximum concrete compression strain (%): 0.00  
 Maximum concrete compression stress (psi): 0  
 Resultant tension force (lb): 1146  
 Resultant compression force (lb): 0  
 Eccentricity of resultant tension forces in x-axis,  $e'_{Nx}$  (inch): 0.00  
 Eccentricity of resultant tension forces in y-axis,  $e'_{Ny}$  (inch): 0.00

### 4. Steel Strength of Anchor in Tension (Sec. 17.4.1)

$N_{sa}$ (lb)	$\phi$	$\phi N_{sa}$ (lb)
13110	0.75	9833

### 5. Concrete Breakout Strength of Anchor in Tension (Sec. 17.4.2)

$$N_b = k_c \lambda_a \sqrt{f'_c} h_{ef}^{1.5} \text{ (Eq. 17.4.2.2a)}$$

$k_c$	$\lambda_a$	$f'_c$ (psi)	$h_{ef}$ (in)	$N_b$ (lb)
17.0	1.00	2500	2.667	3701

$$\phi N_{cb} = \phi (A_{Nc} / A_{Nco}) \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b \text{ (Sec. 17.3.1 \& Eq. 17.4.2.1a)}$$

$A_{Nc}$ (in <sup>2</sup> )	$A_{Nco}$ (in <sup>2</sup> )	$c_{a,min}$ (in)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	$N_b$ (lb)	$\phi$	$\phi N_{cb}$ (lb)
48.00	64.00	2.75	0.906	1.00	1.000	3701	0.65	1635

### 6. Adhesive Strength of Anchor in Tension (Sec. 17.4.5)

$$\tau_{k,cr} = \tau_{k,cr} f_{short-term} K_{sat} (f'_c / 2,500)^n$$

$\tau_{k,cr}$ (psi)	$f_{short-term}$	$K_{sat}$	$f'_c$ (psi)	$n$	$\tau_{k,cr}$ (psi)
1356	1.00	1.00	2500	0.24	1356

$$N_{ba} = \lambda_a \tau_{cr} \pi d_a h_{ef} \text{ (Eq. 17.4.5.2)}$$

$\lambda_a$	$\tau_{cr}$ (psi)	$d_a$ (in)	$h_{ef}$ (in)	$N_{ba}$ (lb)
1.00	1356	0.63	6.000	15975

$$\phi N_a = \phi (A_{Na} / A_{Na0}) \Psi_{ed,Na} \Psi_{cp,Na} N_{ba} \text{ (Sec. 17.3.1 \& Eq. 17.4.5.1a)}$$

$A_{Na}$ (in <sup>2</sup> )	$A_{Na0}$ (in <sup>2</sup> )	$c_{Na}$ (in)	$c_{a,min}$ (in)	$\Psi_{ed,Na}$	$\Psi_{cp,Na}$	$N_{ba}$ (lb)	$\phi$	$\phi N_a$ (lb)
76.57	307.10	8.76	2.75	0.794	1.000	15975	0.65	2056



## 11. Results

### 11. Interaction of Tensile and Shear Forces (Sec. D.7)?

Tension	Factored Load, $N_{ua}$ (lb)	Design Strength, $\phi N_n$ (lb)	Ratio	Status
Steel	1146	9833	0.12	Pass
<b>Concrete breakout</b>	<b>1146</b>	<b>1635</b>	<b>0.70</b>	<b>Pass (Governs)</b>
Adhesive	1146	2056	0.56	Pass

**SET-3G w/ 5/8"Ø F1554 Gr. 36 with hef = 6.000 inch meets the selected design criteria.**

## 12. Warnings

- Minimum spacing and edge distance requirement of  $6d_a$  per ACI 318 Sections 17.7.1 and 17.7.2 for torqued cast-in-place anchor is waived per designer option.
- Designer must exercise own judgement to determine if this design is suitable.
- Refer to manufacturer's product literature for hole cleaning and installation instructions.



# HDU4 (Cast in)

## 1. Project information

Customer company:  
Customer contact name:  
Customer e-mail:  
Comment:

Project description: HDU4 Cast In

LRFD Loads

1.0W = 5069 lb

Location:

Fastening description:

## 2. Input Data & Anchor Parameters

### General

Design method: ACI 318-14  
Units: Imperial units

### Anchor Information:

Anchor type: Cast-in-place  
Material: AB  
Diameter (inch): 0.625  
Effective Embedment depth,  $h_{ef}$  (inch): 6.000  
Anchor category: -  
Anchor ductility: Yes  
 $h_{min}$  (inch): 8.13  
 $C_{min}$  (inch): 1.38  
 $S_{min}$  (inch): 2.50

### Base Material

Concrete: Normal-weight  
Concrete thickness,  $h$  (inch): 9.00  
State: Cracked  
Compressive strength,  $f'_c$  (psi): 2500  
 $\Psi_{c,v}$ : 1.0  
Reinforcement condition: B tension, B shear  
Supplemental reinforcement: Not applicable  
Reinforcement provided at corners: Yes  
Ignore concrete breakout in tension: No  
Ignore concrete breakout in shear: No  
Ignore 6do requirement: Yes  
Build-up grout pad: No

### Recommended Anchor

Anchor Name: PAB Pre-Assembled Anchor Bolt - PAB5 (5/8"Ø)



**Load and Geometry**

Load factor source: ACI 318 Section 5.3

Load combination: not set

Seismic design: No

Anchors subjected to sustained tension: Not applicable

Apply entire shear load at front row: No

Anchors only resisting wind and/or seismic loads: Yes

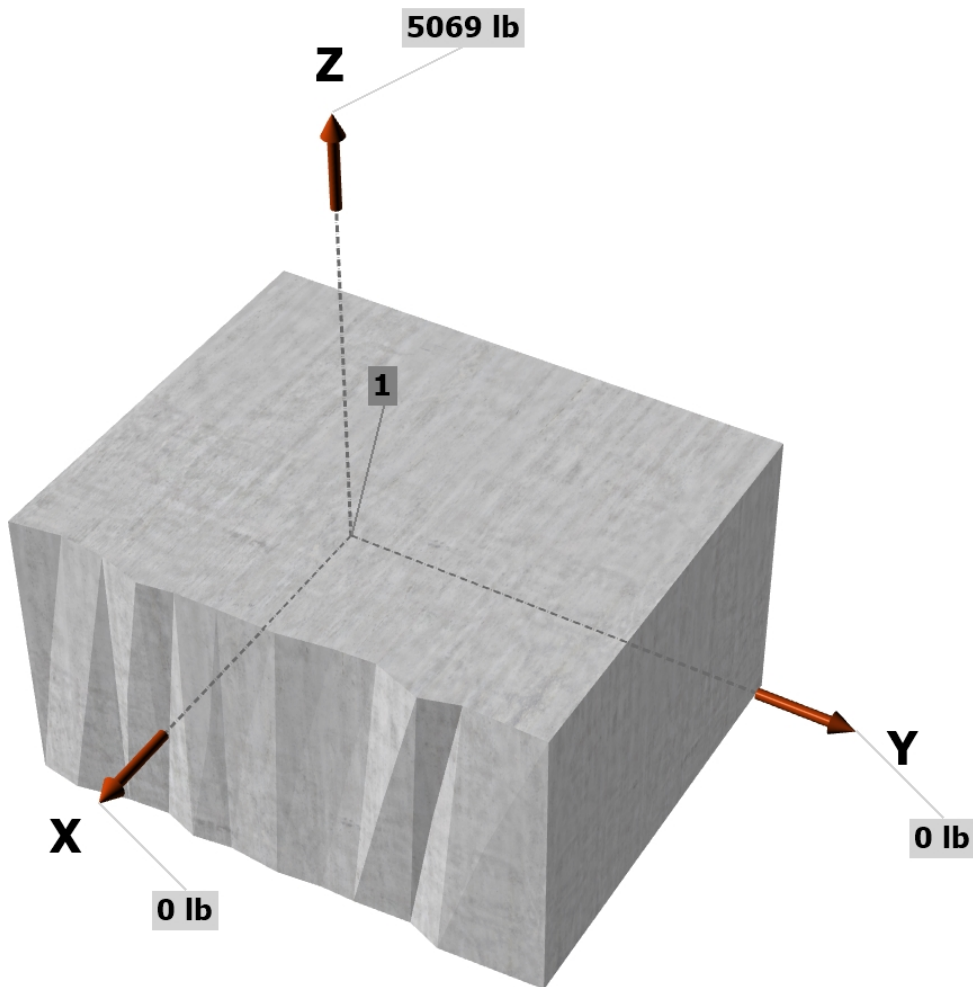
Strength level loads:

$N_{ua}$  [lb]: 5069

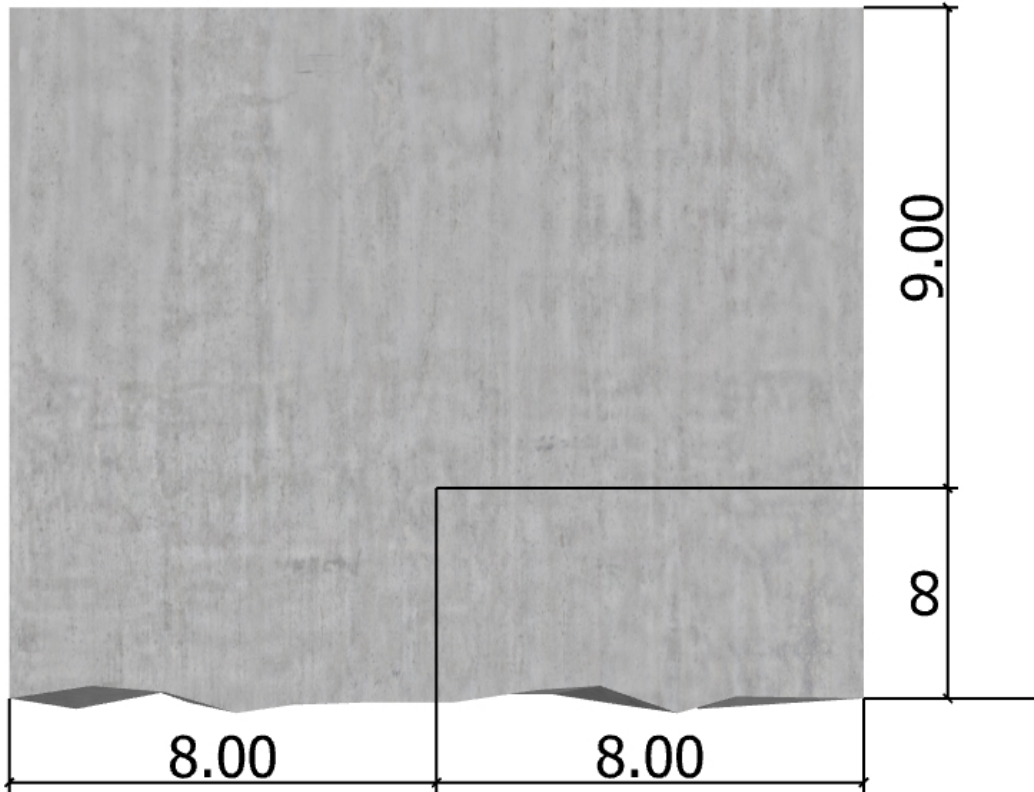
$V_{uax}$  [lb]: 0

$V_{uay}$  [lb]: 0

<Figure 1>



<Figure 2>





### 3. Resulting Anchor Forces

Anchor	Tension load, N <sub>ua</sub> (lb)	Shear load x, V <sub>uax</sub> (lb)	Shear load y, V <sub>uay</sub> (lb)	Shear load combined, $\sqrt{(V_{uax})^2 + (V_{uay})^2}$ (lb)
1	5069.0	0.0	0.0	0.0
Sum	5069.0	0.0	0.0	0.0

Maximum concrete compression strain (%): 0.00  
 Maximum concrete compression stress (psi): 0  
 Resultant tension force (lb): 5069  
 Resultant compression force (lb): 0  
 Eccentricity of resultant tension forces in x-axis, e'<sub>Nx</sub> (inch): 0.00  
 Eccentricity of resultant tension forces in y-axis, e'<sub>Ny</sub> (inch): 0.00

### 4. Steel Strength of Anchor in Tension (Sec. 17.4.1)

N <sub>sa</sub> (lb)	φ	φN <sub>sa</sub> (lb)
13100	0.75	9825

### 5. Concrete Breakout Strength of Anchor in Tension (Sec. 17.4.2)

$$N_b = k_c \lambda_a \sqrt{f_c} h_{ef}^{1.5} \text{ (Eq. 17.4.2.2a)}$$

k <sub>c</sub>	λ <sub>a</sub>	f <sub>c</sub> (psi)	h <sub>ef</sub> (in)	N <sub>b</sub> (lb)
24.0	1.00	2500	6.000	17636

$$\phi N_{cb} = \phi (A_{Nc} / A_{Nco}) \psi_{ed,N} \psi_{c,N} \psi_{cp,N} N_b \text{ (Sec. 17.3.1 \& Eq. 17.4.2.1a)}$$

A <sub>Nc</sub> (in <sup>2</sup> )	A <sub>Nco</sub> (in <sup>2</sup> )	c <sub>a,min</sub> (in)	ψ <sub>ed,N</sub>	ψ <sub>c,N</sub>	ψ <sub>cp,N</sub>	N <sub>b</sub> (lb)	φ	φN <sub>cb</sub> (lb)
302.00	324.00	8.00	0.967	1.00	1.000	17636	0.70	11124

### 6. Pullout Strength of Anchor in Tension (Sec. 17.4.3)

$$\phi N_{pn} = \phi \psi_{c,P} N_p = \phi \psi_{c,P} 8 A_{brg} f_c \text{ (Sec. 17.3.1, Eq. 17.4.3.1 \& 17.4.3.4)}$$

ψ <sub>c,P</sub>	A <sub>brg</sub> (in <sup>2</sup> )	f <sub>c</sub> (psi)	φ	φN <sub>pn</sub> (lb)
1.0	2.10	2500	0.70	29372



**11. Results**

**11. Interaction of Tensile and Shear Forces (Sec. D.7)?**

Tension	Factored Load, $N_{ua}$ (lb)	Design Strength, $\phi N_n$ (lb)	Ratio	Status
<b>Steel</b>	<b>5069</b>	<b>9825</b>	<b>0.52</b>	<b>Pass (Governs)</b>
Concrete breakout	5069	11124	0.46	Pass
Pullout	5069	29372	0.17	Pass

**PAB5 (5/8"Ø) with hef = 6.000 inch meets the selected design criteria.**

**12. Warnings**

- Minimum spacing and edge distance requirement of  $6d_a$  per ACI 318 Sections 17.7.1 and 17.7.2 for torqued cast-in-place anchor is waived per designer option.
- Designer must exercise own judgement to determine if this design is suitable.



# Strongwall Anchors

## 1. Project information

Customer company:  
Customer contact name:  
Customer e-mail:  
Comment:

Project description: Strongwall Cast In Anchors

LRFD Loads

1.0W = 19260 lb

Location:

Fastening description:

## 2. Input Data & Anchor Parameters

### General

Design method: ACI 318-14  
Units: Imperial units

### Anchor Information:

Anchor type: Cast-in-place  
Material: AB  
Diameter (inch): 1.000  
Effective Embedment depth,  $h_{ef}$  (inch): 9.000  
Anchor category: -  
Anchor ductility: Yes  
 $h_{min}$  (inch): 11.63  
 $C_{min}$  (inch): 1.88  
 $S_{min}$  (inch): 4.00

### Base Material

Concrete: Normal-weight  
Concrete thickness,  $h$  (inch): 12.00  
State: Cracked  
Compressive strength,  $f'_c$  (psi): 2500  
 $\Psi_{c,v}$ : 1.0  
Reinforcement condition: B tension, B shear  
Supplemental reinforcement: Not applicable  
Reinforcement provided at corners: Yes  
Ignore concrete breakout in tension: No  
Ignore concrete breakout in shear: No  
Ignore 6do requirement: Yes  
Build-up grout pad: No

### Recommended Anchor

Anchor Name: PAB Pre-Assembled Anchor Bolt - PAB8 (1"Ø)



**Load and Geometry**

Load factor source: ACI 318 Section 5.3

Load combination: not set

Seismic design: No

Anchors subjected to sustained tension: Not applicable

Apply entire shear load at front row: No

Anchors only resisting wind and/or seismic loads: Yes

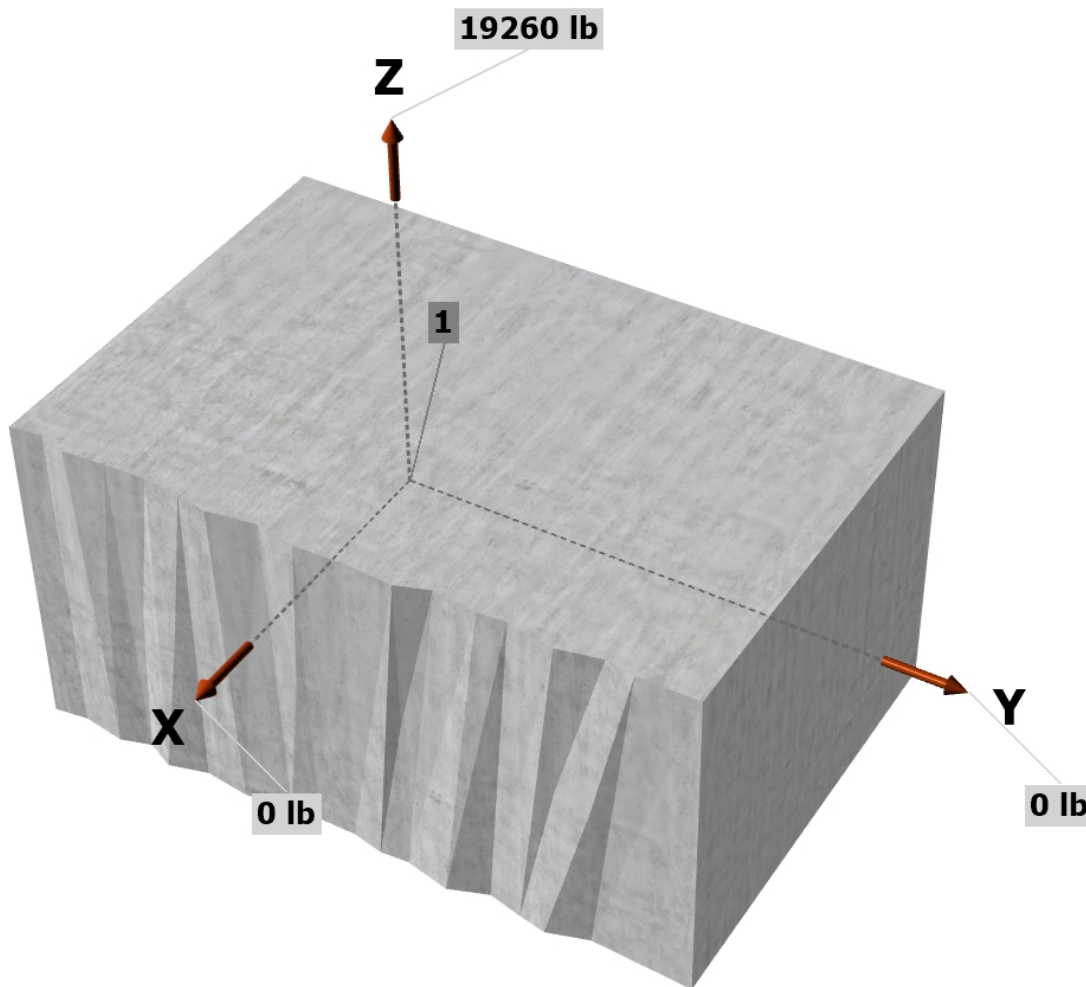
Strength level loads:

$N_{ua}$  [lb]: 19260

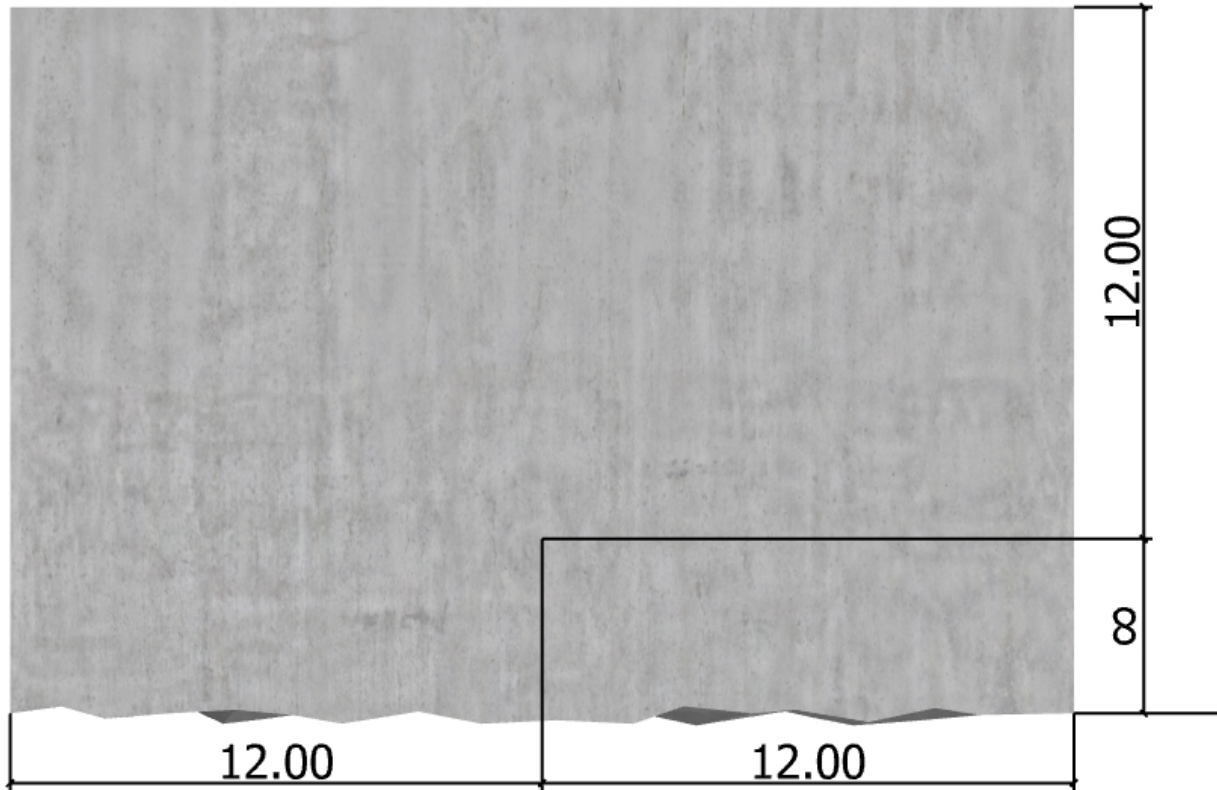
$V_{uax}$  [lb]: 0

$V_{uay}$  [lb]: 0

<Figure 1>



<Figure 2>





### 3. Resulting Anchor Forces

Anchor	Tension load, N <sub>ua</sub> (lb)	Shear load x, V <sub>uax</sub> (lb)	Shear load y, V <sub>uay</sub> (lb)	Shear load combined, $\sqrt{(V_{uax})^2 + (V_{uay})^2}$ (lb)
1	19260.0	0.0	0.0	0.0
Sum	19260.0	0.0	0.0	0.0

Maximum concrete compression strain (%): 0.00  
 Maximum concrete compression stress (psi): 0  
 Resultant tension force (lb): 19260  
 Resultant compression force (lb): 0  
 Eccentricity of resultant tension forces in x-axis, e'<sub>Nx</sub> (inch): 0.00  
 Eccentricity of resultant tension forces in y-axis, e'<sub>Ny</sub> (inch): 0.00

### 4. Steel Strength of Anchor in Tension (Sec. 17.4.1)

N <sub>sa</sub> (lb)	φ	φN <sub>sa</sub> (lb)
35150	0.75	26363

### 5. Concrete Breakout Strength of Anchor in Tension (Sec. 17.4.2)

$$N_b = k_c \lambda_a \sqrt{f_c} h_{ef}^{1.5} \text{ (Eq. 17.4.2.2a)}$$

k <sub>c</sub>	λ <sub>a</sub>	f <sub>c</sub> (psi)	h <sub>ef</sub> (in)	N <sub>b</sub> (lb)
24.0	1.00	2500	8.000	27153

$$\phi N_{cb} = \phi (A_{Nc} / A_{Nco}) \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b \text{ (Sec. 17.3.1 \& Eq. 17.4.2.1a)}$$

A <sub>Nc</sub> (in <sup>2</sup> )	A <sub>Nco</sub> (in <sup>2</sup> )	c <sub>a,min</sub> (in)	Ψ <sub>ed,N</sub>	Ψ <sub>c,N</sub>	Ψ <sub>cp,N</sub>	N <sub>b</sub> (lb)	φ	φN <sub>cb</sub> (lb)
609.00	576.00	12.00	1.000	1.00	1.000	27153	0.70	20096

### 6. Pullout Strength of Anchor in Tension (Sec. 17.4.3)

$$\phi N_{pn} = \phi \Psi_{c,P} N_p = \phi \Psi_{c,P} 8 A_{brg} f_c \text{ (Sec. 17.3.1, Eq. 17.4.3.1 \& 17.4.3.4)}$$

Ψ <sub>c,P</sub>	A <sub>brg</sub> (in <sup>2</sup> )	f <sub>c</sub> (psi)	φ	φN <sub>pn</sub> (lb)
1.0	5.15	2500	0.70	72156



**11. Results**

**11. Interaction of Tensile and Shear Forces (Sec. D.7)?**

Tension	Factored Load, $N_{ua}$ (lb)	Design Strength, $\phi N_n$ (lb)	Ratio	Status
Steel	19260	26363	0.73	Pass
<b>Concrete breakout</b>	<b>19260</b>	<b>20096</b>	<b>0.96</b>	<b>Pass (Governs)</b>
Pullout	19260	72156	0.27	Pass

**PAB8 (1"Ø) with hef = 9.000 inch meets the selected design criteria.**

**12. Warnings**

- Minimum spacing and edge distance requirement of  $6d_a$  per ACI 318 Sections 17.7.1 and 17.7.2 for torqued cast-in-place anchor is waived per designer option.
- Designer must exercise own judgement to determine if this design is suitable.

## FOOTING WITH COMBINED AXIAL AND FLEXURAL LOADS

### FOOTING UNDER STRONGWALL

#### Sizes and Loads:

##### superstructure:

wall 3,626 lb

##### footing:

length 11.50 ft (along same axis as applied moment)  
width 2.00 ft (perpendicular to applied moment)  
depth 1.00 ft  
weight 3,335 lb

soil abv. 0 lb

total R = 6,961 lb

M = 17,420 lbft

e = 2.50 ft

B/6 = 1.92 ft

#### Bearing Pressures:

Reaction is OUTSIDE kern.

(Use these results)

(Do not use these results)

x = 3.25 ft

fa = 303 psf

fb = 395 psf

fp = 715 psf

fp = 698 psf

Fa = 2,000 psf

Fa = 2,000 psf

#### Stability:

Mot = 17,420 lbft (using 0.7E, per ASD Load Combinations)

Mr = 24,015 lbft (using 0.6D, per ASD Load Combinations)